QCX-20 Low Output Power Problem Low-pass Filter Design Part 1

The Symptoms

After building and testing my QCX-20, I observed that the output power was significantly lower than indicated by the graph on page 138 of the Rev-4f manual. With 13 volts applied (voltage after D3), the QCX-20 output measured 2.5 watts vs 3.9 watts on the graph. My QCX-40 output measured 3.4 watts vs 3.7 watts on the graph, which is a reasonable difference.

Because low output power on the QCX-20 seems to be a common problem, I decided to do some further investigation. The measured output power of the QCX-40 at different frequencies across the 40 meter band was nearly constant. However, the measured output power of the QCX-20, varied inversely with frequency.

Plotting the peak output voltage (instead of power) from the QCX-20 across a 50 ohm load versus frequency gave a straight line. This suggested that the operating frequency was too close to the knee of the low-pass filter. The slope of the plotted line was 11 volts / MHz. With this information, I calculated how much the low-pass filter cutoff frequency would need to be increased to get 4 watts out across the entire band, as follows.

Peak voltage required for 4 watts across 50 ohms = 20 volts Peak voltage measured at 14.350 MHz (the top of the 20 meter band) = 12.2 volts Required increase in filter frequency $(20 V - 12.2 V) / (11 V / MHz) = 0.709 MHz$

Although only 5% of the operating frequency, this required frequency change seems too large to be simply a symptom of component tolerances, particularly when considering the number of users experiencing the problem. Therefore, I decided to do further analysis of the low-pass filter.

Analysis of Filter Sources

My first stop was "A short guide to harmonic filter for QRP transmitter output" by G3RJV [\(http://www.gqrp.com/harmonic_filters.pdf\)](http://www.gqrp.com/harmonic_filters.pdf), which is the source for the low-pass filter component values used in the QCX transceivers.

The spread sheet (below) shows the filter data from TABLE 1 of this article. Columns highlighted in purple are added to assist with the analysis.

The first added column is the difference between the top of each band and the corresponding F-co (ripple cutoff frequency). Apparently, F-co is not necessarily the frequency of no attenuation (see graph below). Highlighted in yellow are differences that seem low (less than 0.1 MHz), one of which is 20 meters. Highlighted in orange are differences that seem high.

The second added column is the ratio of F-3dB (frequency of 3dB attenuation) for each band and the corresponding F-co. Highlighted in yellow are the lower ratios, including 20 meters. The lower ratio indicates the 3dB point is closer to F-co, suggesting that part of the pass-band is more likely to be attenuated. The average ratio is in blue. Ratios less than 1.2 were of concern.

The third added column is the $2nd$ harmonic of the bottom frequency of each band, which is what needs to be attenuated. The corresponding F-30dB frequencies that are higher than the $2nd$ harmonic are highlighted.

With these concerns, I decide to go to the source of this information which is a 2-part article by W3NQN. This article, "Low-pass Filters for Attenuating RF Amplifier Harmonics," can be found split between the December 1983 and January 1984 issues of The Short Wave Magazine [\(https://www.americanradiohistory.com/Short_Wave_UK.htm](https://www.americanradiohistory.com/Short_Wave_UK.htm)).

In his article, W3NQN describes several 5-element low-pass filters and argues for the use of a 7-element Chebyshev low-pass filter for solid state amplifiers. The article is worth reading, but the most relevant part is a list of 30 pre-designed filters using standard-value capacitors, which is where G3RJV obtained the filter data for TABLE 1.

Figure 2 (below) of the W3NQN article shows the schematic of the 7-element filter and graph of attenuation vs frequency. The component designators in this schematic are used for most of the following discussion.

Looking at the list of 30 filters, I did my own selection of a filter for each Ham band. The following criteria were used to make the selections, prioritizing in the order listed, but in a few cases compromises were made.

- 1) F-3dB / F-co should be 1.2 or greater to reduce the possibility of attenuation in the pass band.
- 2) F-30dB should be less than the 2^{nd} harmonic to ensure more than 30dB attenuation of the 2^{nd} harmonic.
- 3) F-co Top (of the band) should be a minimum

The rows highlighted in green are changed from the original table. The following are a few items to note.

- 1) For 20, 80, and 160 meters, F-3dB / F-co is less than 1.2, but only 80 meters is significantly less and needs testing.
- 2) For 160 meters, F-30dB is not less than the $2nd$ harmonic frequency because no better option is available.
- 3) For 10, 12, and 17 meters, the differences between F-co and the top frequency are relatively large because no better options are available.

Note that F-3dB for 20 meters increased from 16.410 MHz to 17.260 MHz, a difference of 0.850 MHz. Previously, an increase of the filter frequency to obtain an output of 4 watts across the entire band was calculated to be 0.709 MHz. Therefore, these new component values for 20 meters should work.

Below is a list of the capacitor and inductor values for the selected filters. The component designators refer to the schematic in figure 2 from the W3NQN article, not the QCX schematic.

For the QCX-20, the number of turns for L2, L4, and L6 remain the same as the current QCX design. However, the capacitors are reduced.

The list of 30 filters in the W3NQN article also provided VSWR data. The filters on the list were selected from a larger list because they have a VSWR of about 1.1:1 or less. From the W3NQN data, my selected Ham band filters all have a VSWR of 1.07:1 or less.

Conclusion and Test

The table below shows the component values for 20 and 40 meter W3NQN low-pass filters. The values currently used in the QCX design are on the left, and the revised filters are on the right. The component designators are from the W3NQN schematic.

Using the revised filter for 20 meters requires reducing the capacitor values as highlighted in green. The turns for L2 and L6 in the QCX-40 are highlighted in yellow because, by calculation, these toroids require 21.6 turns, which would normally be rounded up to 22 turns. However, as specified in the QCX manual, I used 21 turns when I built the QCX-40, and it works great.

Before completing this analysis, I modified the QCX-20 by removing one turn from L1 and L3 (QCX schematic designators), as recommended on the QRP Labs web site. The resulting performance provided a constant appropriate output power across all but the top of the 20 meter band. As the CW / lower half of the band was operating normally and 150 pF capacitors were not readily available at that time, I stayed with this modification.

After completing this analysis, I purchased some 150 pF NP0 capacitors, and modified the QCX-20 by rewinding L1 and L3 with the original 16 turns and changing C25 – C28 (QCX schematic designators) per the values highlighted in green. The resulting performance provided a nearly constant 3.5 watts across the entire 20 meter band. Although slightly less than the 3.9 watts on the graph in the manual, this output seems appropriate.

To be continued

In part 2, the revised list of W3NQN low-pass filters will be further analyzed. Also, a number of parameters will be considered to develop a worst-case design for low-pass filters.